

(12) **United States Patent**
Yakita

(10) **Patent No.:** **US 9,104,017 B2**
(45) **Date of Patent:** **Aug. 11, 2015**

(54) **ZOOM LENS AND IMAGE PICKUP APPARATUS INCLUDING THE SAME**

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(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

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(21) Appl. No.: **14/259,217**

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(22) Filed: **Apr. 23, 2014**

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(65) **Prior Publication Data**

US 2014/0320977 A1 Oct. 30, 2014

(30) **Foreign Application Priority Data**

Apr. 30, 2013 (JP) 2013-095318

(51) **Int. Cl.**
G02B 15/177 (2006.01)

(52) **U.S. Cl.**
CPC **G02B 15/177** (2013.01)

(58) **Field of Classification Search**
CPC G02B 15/177; G02B 9/34; G02B 9/36
See application file for complete search history.

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(57) **ABSTRACT**

A zoom lens includes in order from an object side: a positive first lens unit; a negative second lens unit which moves during zooming; a third lens unit; a stop; and a positive fourth lens unit. The first lens unit includes, in order from the object side, a negative first lens subunit which does not move, a positive second lens subunit which moves during focusing, and a positive third lens subunit which does not move. The first lens subunit is composed of one or more negative lenses, and the second lens subunit includes a positive lens and a negative lens. An average value of Abbe constants of the first lens subunit, an average value of Abbe constants of the positive lenses of the second lens subunit, and an average value of Abbe constants of the negative lenses of the second lens subunit are appropriately set.

6 Claims, 9 Drawing Sheets

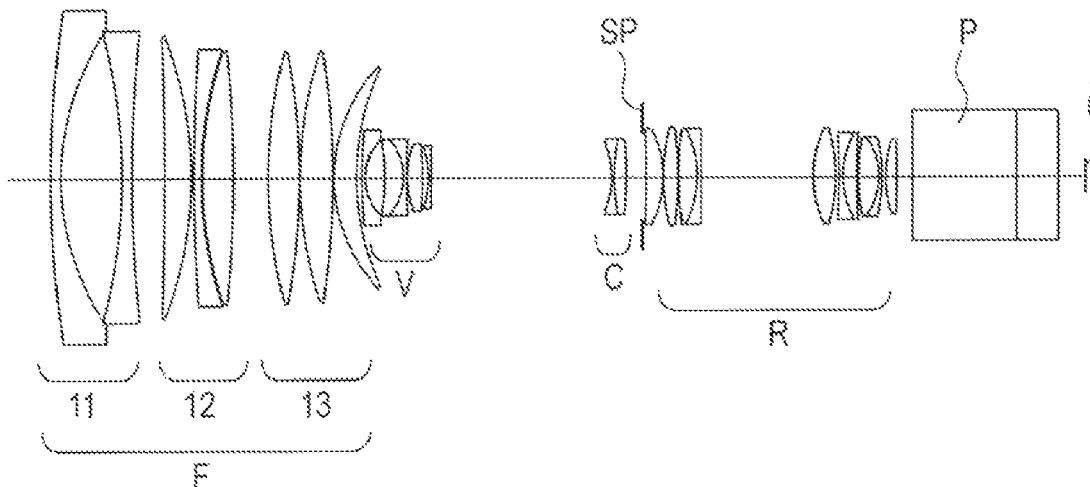


FIG. 1

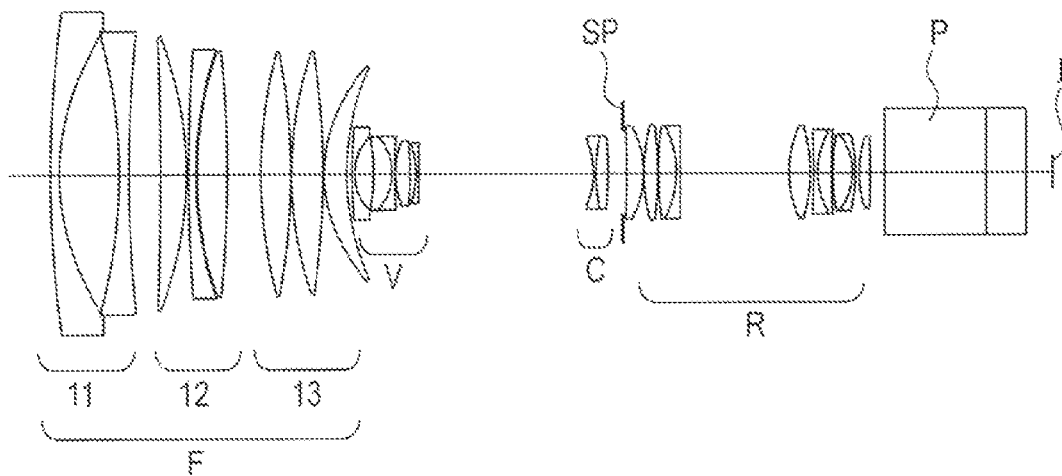


FIG. 2

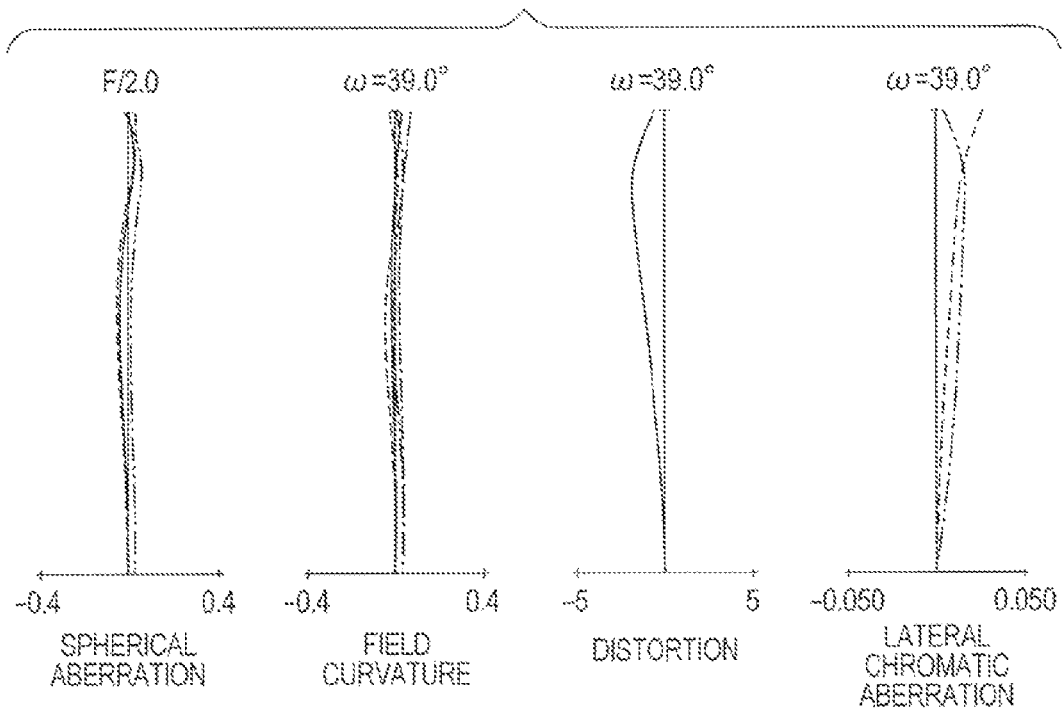


FIG. 3

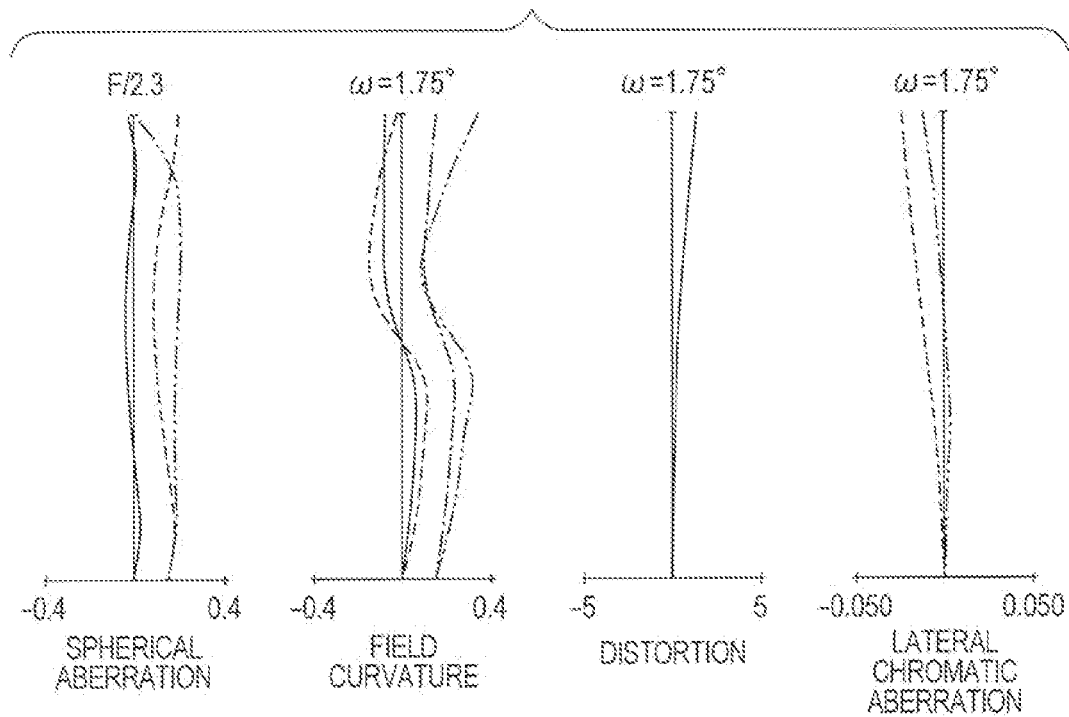


FIG. 4

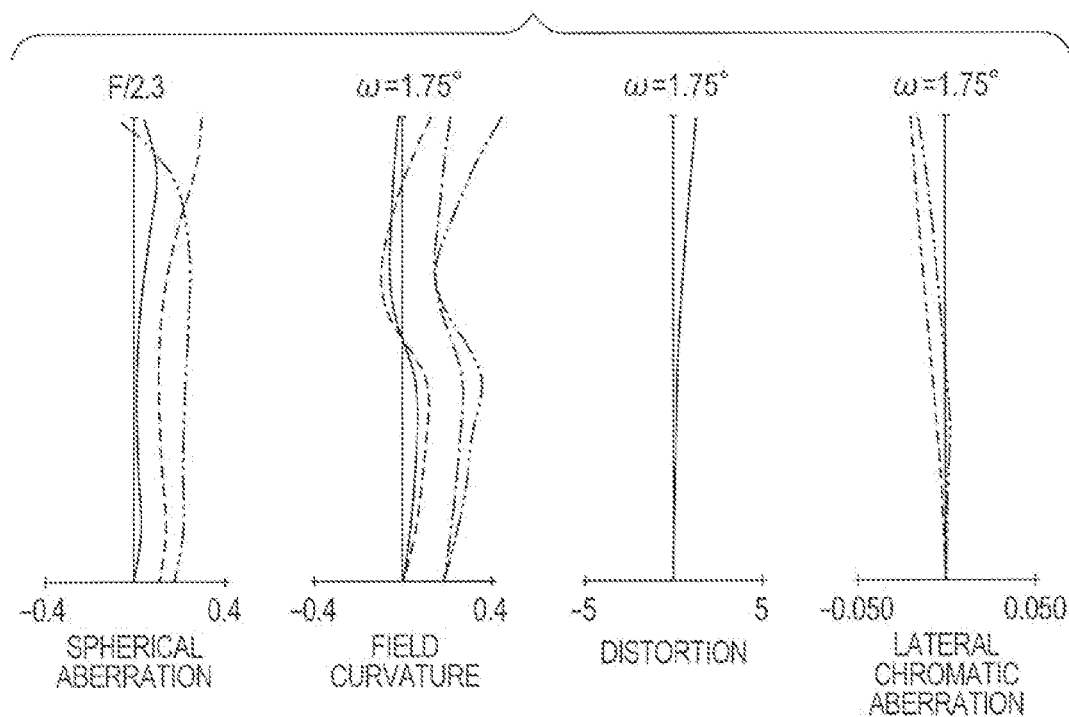


FIG. 5

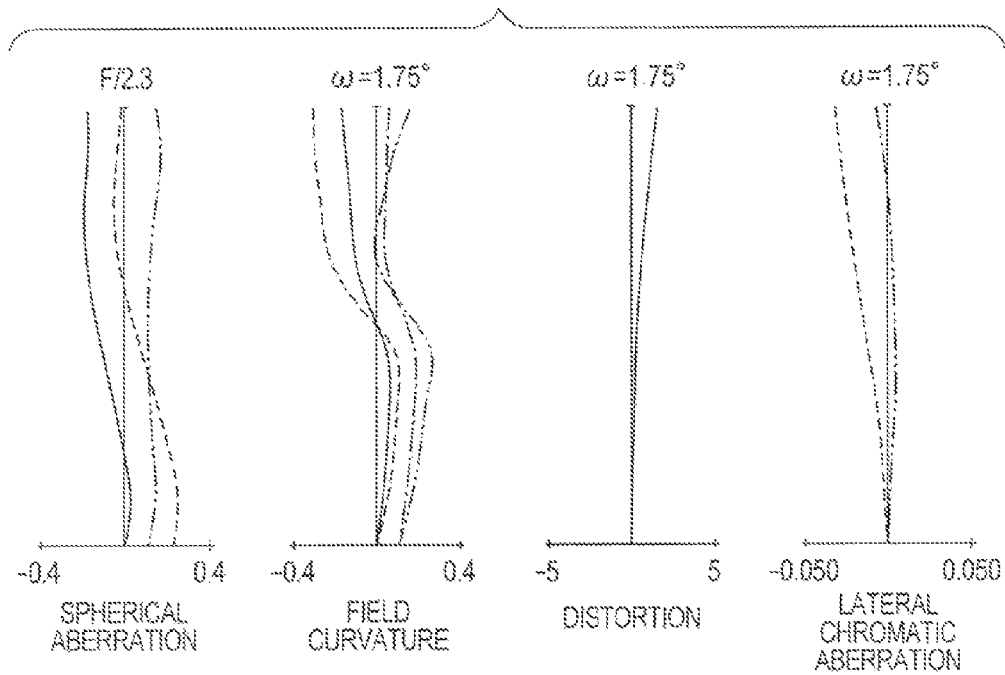


FIG. 6

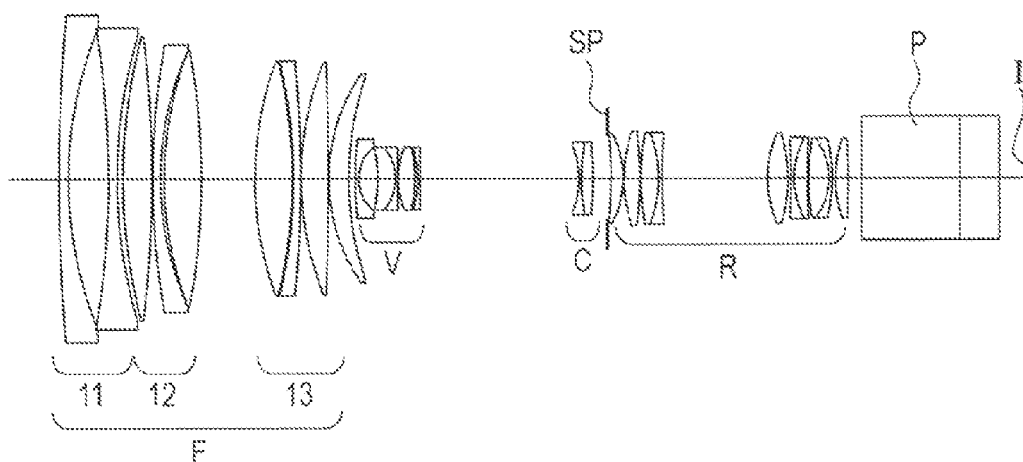


FIG. 7

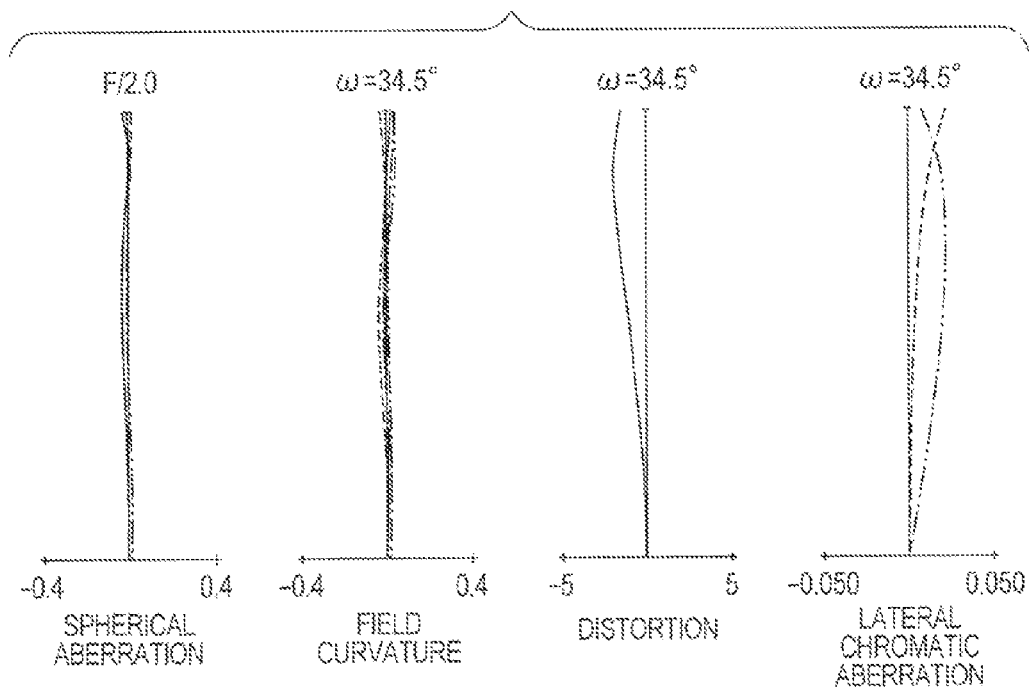


FIG. 8

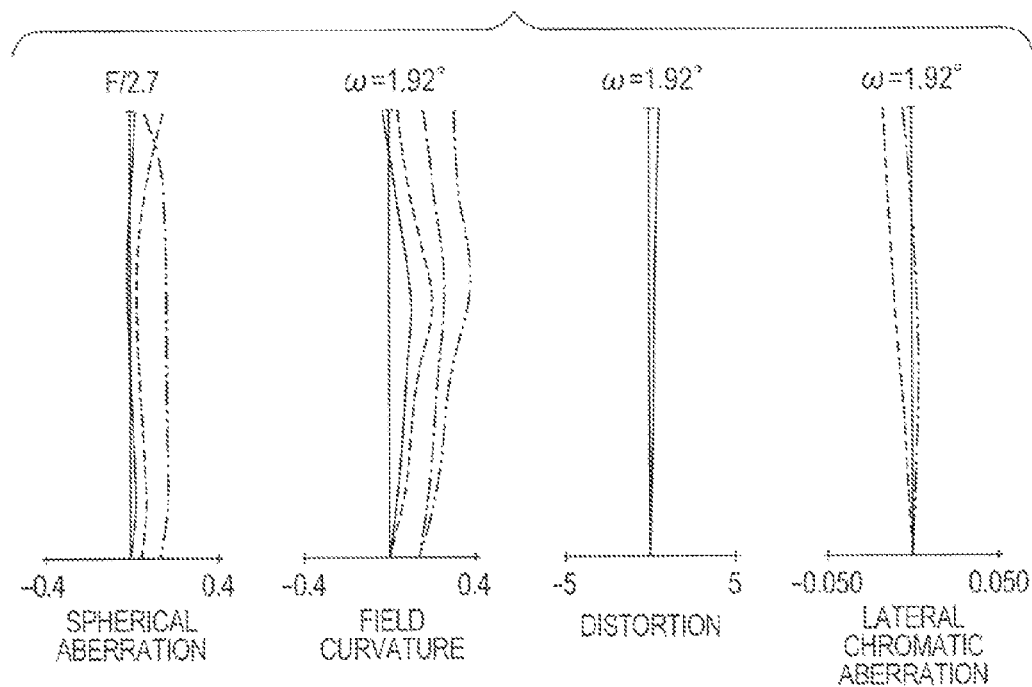


FIG. 9

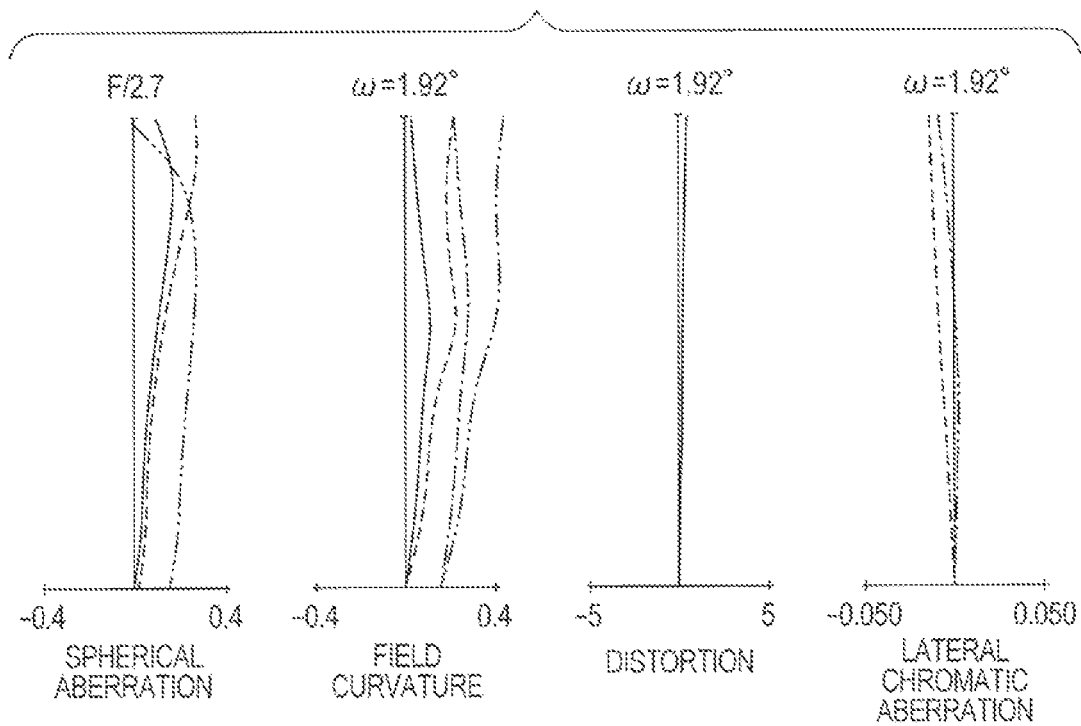


FIG. 10

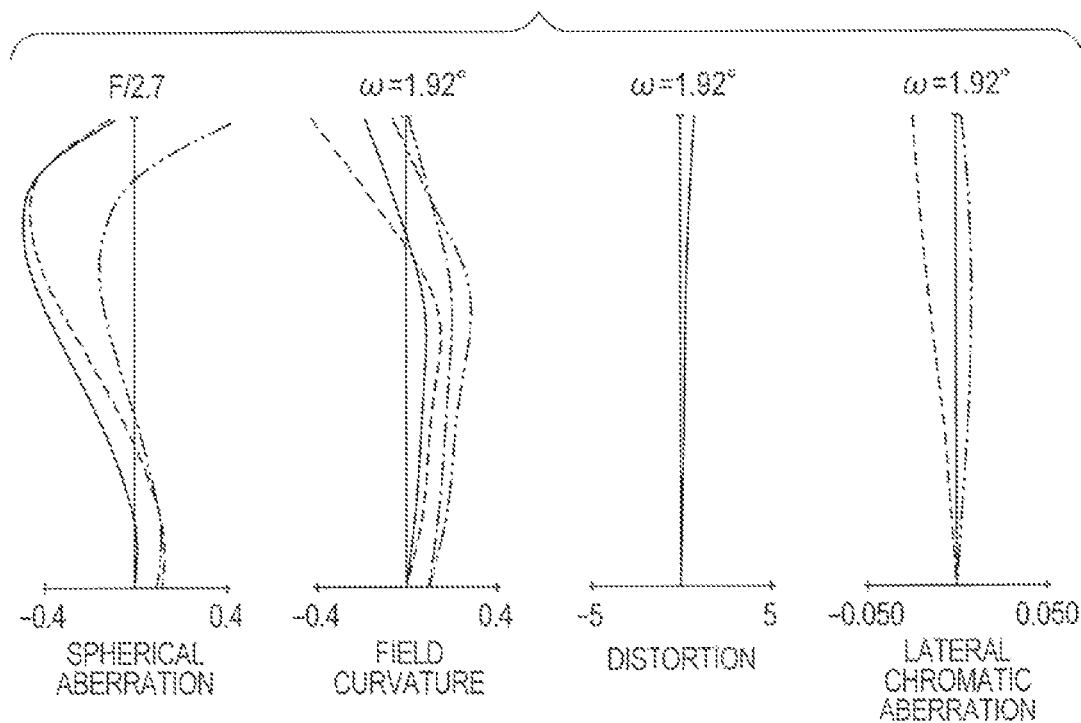


FIG. 11

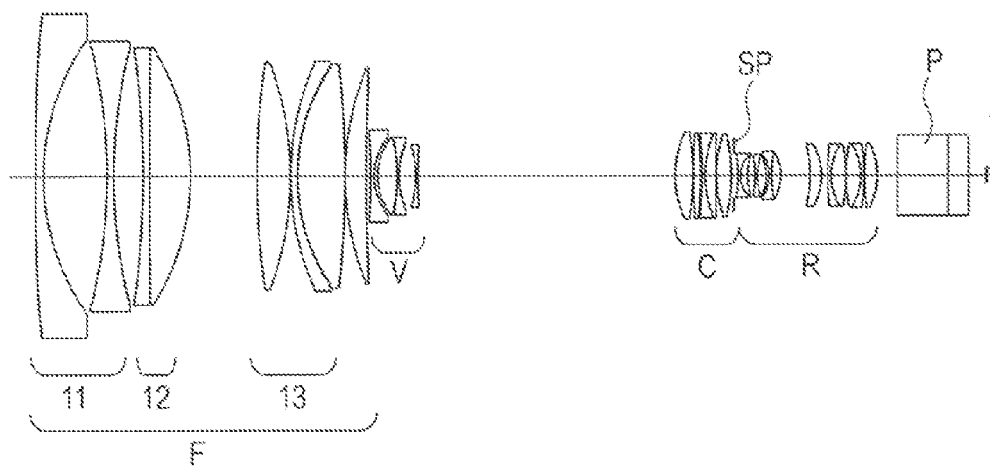


FIG. 12

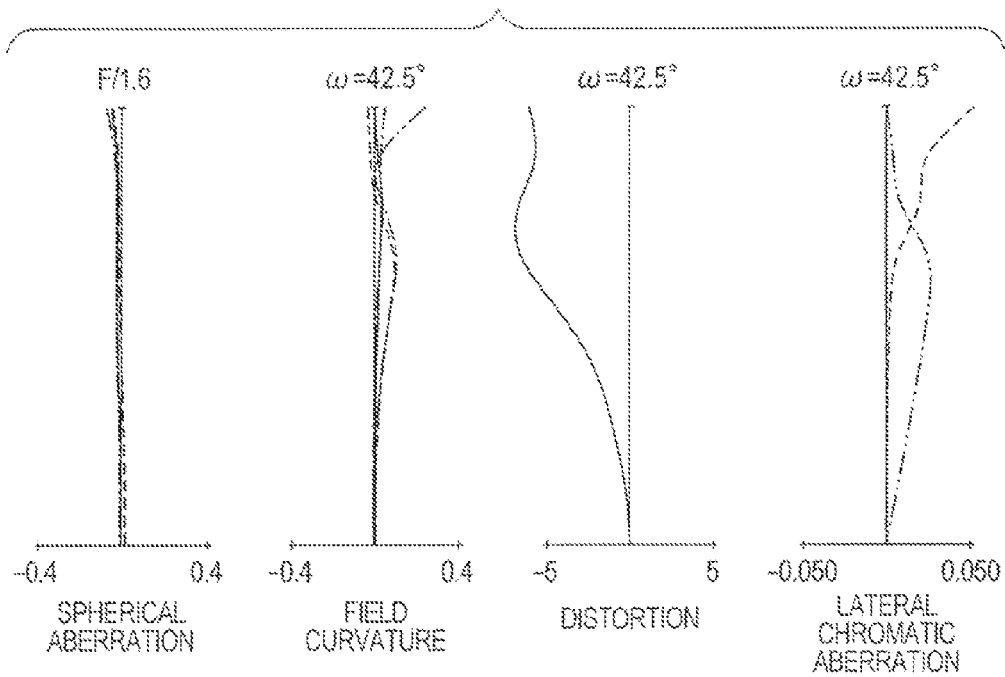


FIG. 13

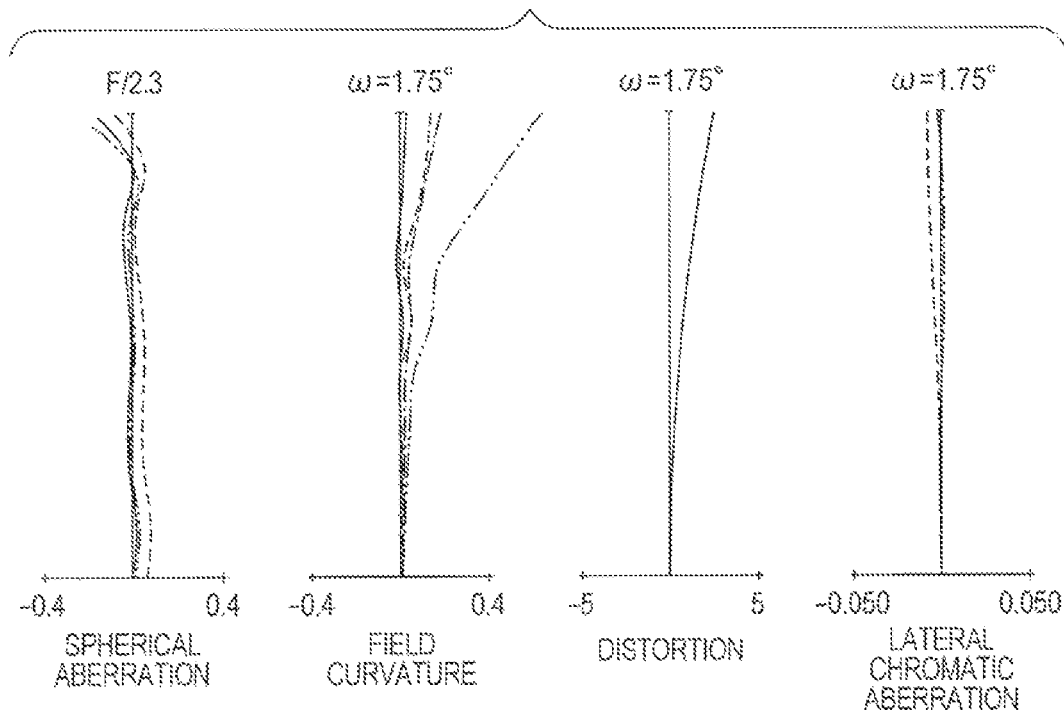


FIG. 14

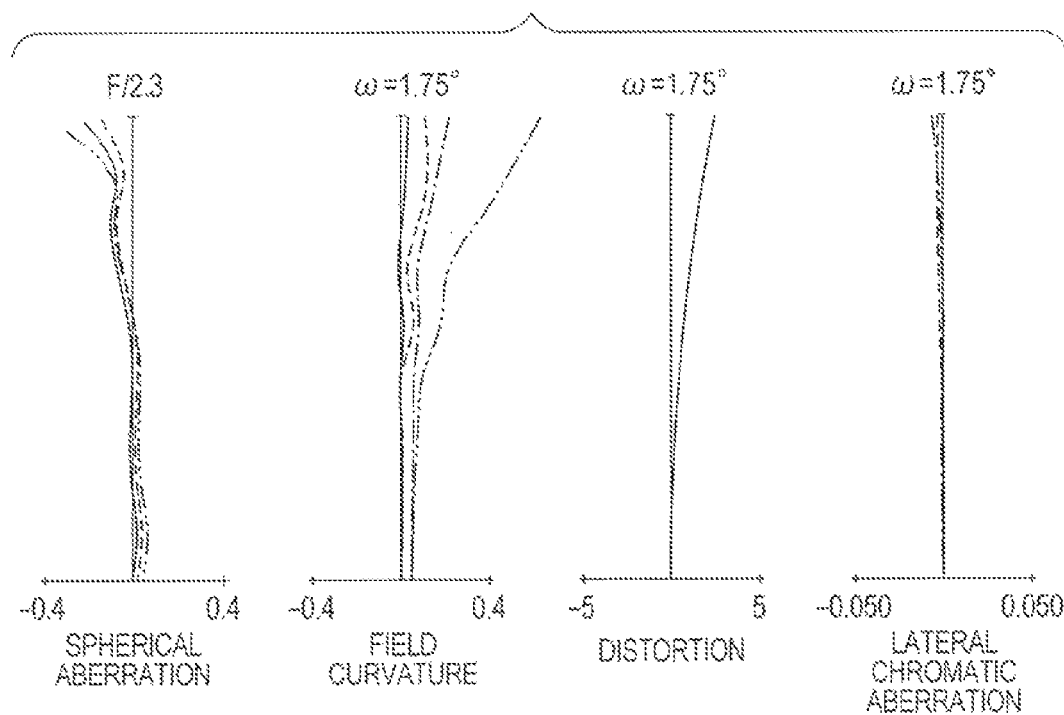


FIG. 15

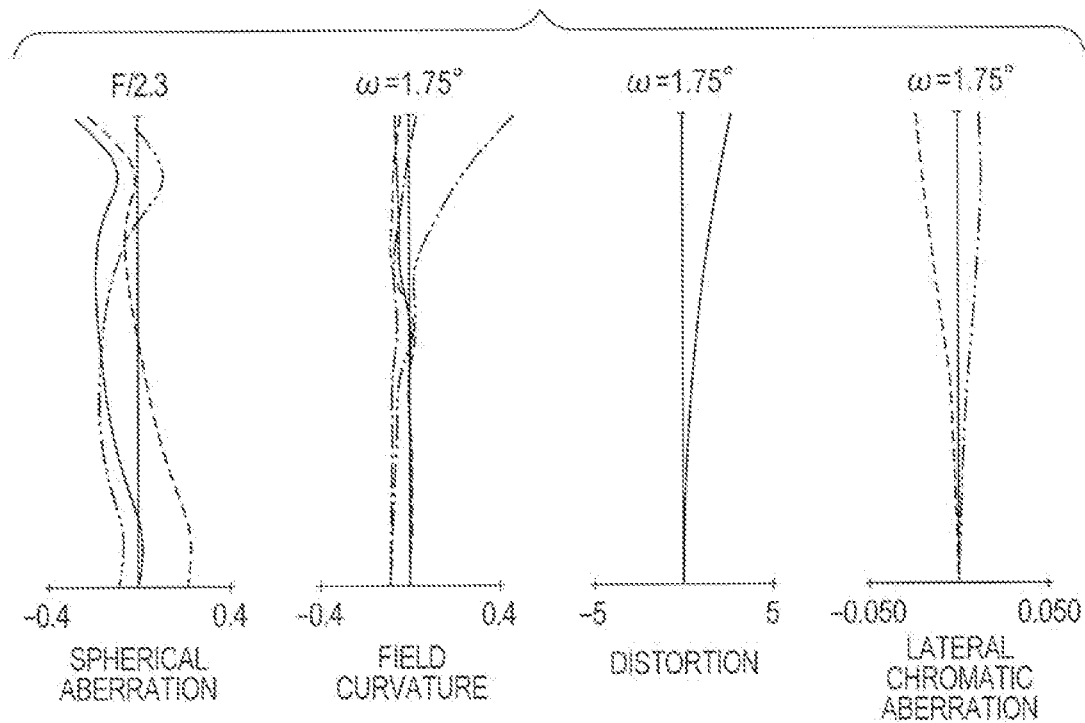


FIG. 16

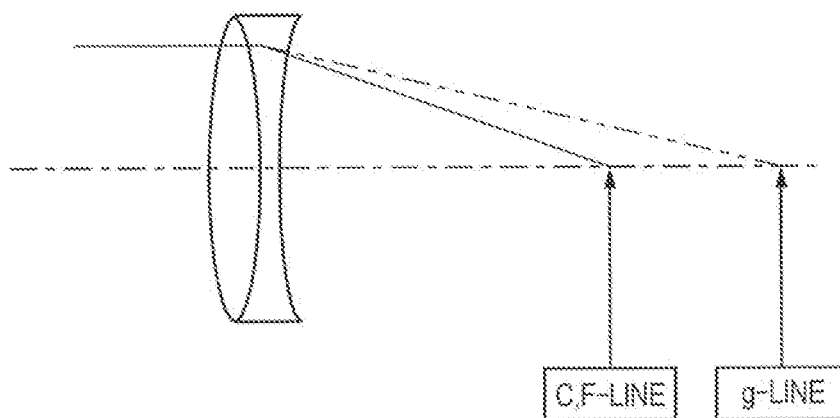
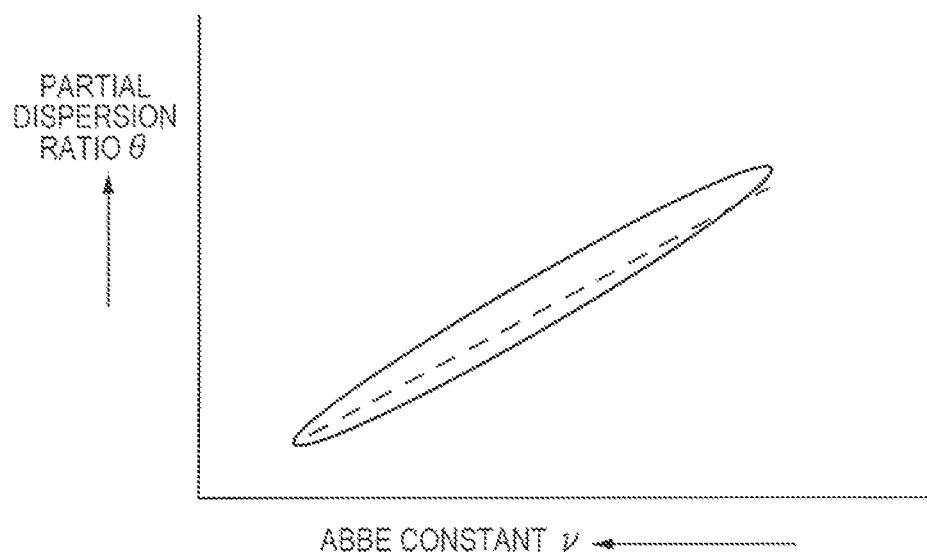


FIG. 17



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ZOOM LENS AND IMAGE PICKUP APPARATUS INCLUDING THE SAME

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to a zoom lens which is suitable for use in a broadcasting television camera, a video camera, a digital still camera, and a silver-halide film camera, and also to an image pickup apparatus including the zoom lens.

2. Description of the Related Art

Hitherto, for an image pickup apparatus such as a television camera, a silver-halide film camera, a digital camera, and a video camera, there is proposed a zoom lens including, in order from an object side to an image side, a positive first lens unit having a focus unit, a negative second lens unit for zooming, a positive or negative third lens unit for correcting image plane variation due to the zooming, and a positive fourth lens unit for image formation.

In particular, there is proposed a zoom lens in which the first lens unit includes, in order from the object side to the image side, a fixed negative first lens subunit, a positive second lens subunit for focusing, and a fixed positive third lens subunit, which is advantageous for suppressing a variation of performance depending on an object distance, suppressing a variation of an angle of field due to focusing, and achieving a wider angle of field.

Japanese Patent Application Laid-Open No. H09-15501 discloses an embodiment having an angle of field of 78° or smaller at a wide angle end. The first lens subunit includes at least one positive lens, and the second lens subunit includes at least one positive lens and a cemented lens, so as to achieve good optical performance over the entire zoom range and the entire object distance range.

Japanese Patent Application Laid-Open No. 2009-42346 discloses an embodiment having an angle of field of 99° or smaller at the wide angle end. An aspherical lens is appropriately disposed in the second lens subunit, so as to obtain high optical performance over the entire object distance range.

Japanese Patent Application Laid-Open No. 2000-321496 discloses an embodiment having an angle of field of 78° or smaller at the wide angle end. Aspherical lenses are disposed in the first lens subunit and in the third lens subunit, so as to achieve high optical performance over the entire zoom range.

Japanese Patent Application Laid-Open No. 2001-21804 discloses an embodiment having an angle of field of 78° or smaller at the wide angle end. Aspherical lenses are disposed in the second lens subunit and in the third lens subunit, and refractive powers of the first lens subunit to the third lens subunit are appropriately set, so as to achieve high optical performance over the entire focus range.

Japanese Patent Application Laid-Open No. 2001-116993 discloses an embodiment having an angle of field of 74° or smaller at the wide angle end. Lateral magnifications and focal lengths of individual lens units are appropriately set, so as to achieve a reduction of a variation of an angle of field due to focusing.

Japanese Patent Application Laid-Open No. 2012-113139 discloses an embodiment having an angle of field of 75° or smaller at the wide angle end. Refractive powers and glass types of the first lens unit and the second lens unit are appropriately set, so as to achieve a wide angle of field, a high zoom ratio, and high optical performance over the entire zoom range.

Japanese Patent Application Laid-Open No. 2005-249974 discloses an embodiment having an angle of field of 81° or

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smaller at the wide angle end. Lens configurations of the first lens subunit, the second lens subunit, and the third lens subunit are appropriately set, so as to achieve reductions in size and weight of the first lens unit while maintaining high optical performance.

Japanese Patent Application Laid-Open No. H10-31157 discloses an embodiment having an angle of field of 75° or smaller at the wide angle end. The second lens unit is divided into a second lens unit A and a second lens unit B, and an interval between the lens units is changed in zooming, so as to achieve reductions in size and weight of the entire lens system while maintaining a variation of performance to be small over the entire zoom range and the entire focus range.

Japanese Patent Application Laid-Open No. H06-242378 discloses an embodiment having an angle of field of 64° or smaller at the wide angle end. Focal lengths and glass types of the first lens subunit and the second lens subunit are appropriately set, so as to achieve a lens unit having a high zoom ratio, a wide angle of field, and a short distance at close range.

In Japanese Patent Application Laid-Open No. H09-15501 and Numerical Embodiments 1 and 2 of Japanese Patent Application Laid-Open No. H06-242378, in order to maintain high optical performance over the entire zoom range and the entire focus range even when a wider angle of field and a higher zoom ratio are achieved, the first lens subunit includes at least three lenses in total including one positive lens and two negative lenses.

In addition, in Numerical Embodiment 3 of Japanese Patent Application Laid-Open No. H06-242378, the first lens subunit includes two negative lenses, and the second lens subunit includes one positive lens and one cemented lens. The first lens subunit has a relatively simple structure, but it is difficult to suppress a variation of axial chromatic aberration over the entire focus range.

SUMMARY OF THE INVENTION

Therefore, the present invention provides a small size and light weight zoom lens, which is optimal for a high magnification zoom lens for broadcasting in particular, and has a simple structure of a first lens unit and good optical performance with suppressed variation over the entire focus range from an object at infinity to a short distance object, and to provide an image pickup apparatus including the zoom lens.

According to one embodiment of the present invention, there are provided a zoom lens and an image pickup apparatus including the zoom lens, including, in order from an object side to an image side: a first lens unit having a positive refractive power; a second lens unit having a negative refractive power which moves during zooming; a third lens unit; a stop; and a fourth lens unit having a positive refractive power. The first lens unit includes, in order from the object side to the image side, a first lens subunit having a negative refractive power which does not move, a second lens subunit having a positive refractive power which moves during focusing, and a third lens subunit having a positive refractive power which does not move. The first lens subunit is composed of one or more negative lenses, and the second lens subunit includes at least one positive lens and at least one negative lens. The following expression is satisfied:

$$9 \times 10^6 < v11a^3 \times (v12ap - v12an) < 45 \times 10^6,$$

where v11a represents an average value of Abbe constants of the first lens subunit, v12ap represents an average value of Abbe constants of the at least one positive lens of the second lens subunit, v12an represents an average value of Abbe

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constants of the at least one negative lens of the second lens subunit, and Abbe constant v is defined as,

$$v=(Nd-1)/(NF-NC)$$

where NF represents a refractive index for F-line, Nd represents a refractive index for d-line, and NC represents a refractive index for C-line.

It is preferred that in the zoom lens and the image pickup apparatus including the zoom lens according to one embodiment of the present invention, the following expressions be satisfied:

$$1.8<\phi_{11}/\phi_{12}<7.0, \text{ and}$$

$$0.5<\phi_{11}/\phi_1<1.0,$$

where ϕ_{11} represents a refractive power of the first lens subunit, ϕ_{12} represents a refractive power of the second lens subunit, and ϕ_1 represents a refractive power of the first lens unit.

It is preferred that in the zoom lens and the image pickup apparatus including the zoom lens according to one embodiment of the present invention, the following expression be satisfied:

$$0.020<\theta_{11a} \times (\theta_{12an} - \theta_{12ap}) < 0.046,$$

where θ_{11a} represents an average value of partial dispersion ratios of the first lens subunit, θ_{12ap} represents an average value of partial dispersion ratios of the at least one positive lens of the second lens subunit, and θ_{12an} represents an average value of partial dispersion ratios of the at least one negative lens of the second lens subunit. Note that, a partial dispersion ratio $\theta=(Ng-NF)/(NF-NC)$ holds, where NF represents a refractive index for F-line, Ng represents a refractive index for g-line, and NC represents a refractive index for C-line.

It is more preferred that in the zoom lens and the image pickup apparatus including the zoom lens according to one embodiment of the present invention, the following expressions be satisfied:

$$0.5<v_{11a}/(v_{13ap}-v_{13an})<4.0, \text{ and}$$

$$0.6<\phi_{13}/\phi_1<1.5,$$

where ϕ_{13} represents a refractive power of the third lens subunit, and v_{13a} represents an average value of Abbe constants of the third lens subunit.

In addition, it is preferred that the following expression be satisfied:

$$0.15<|\phi_1/\phi_2|<0.30,$$

where ϕ_2 represents a refractive power of the second lens unit.

Further features of the present invention will become apparent from the following description of exemplary embodiments with reference to the attached drawings.

According to one embodiment of the present invention, it is possible to provide the small size and light weight zoom lens having a simple structure of the first lens unit and good optical performance with suppressed variation over the entire focus range from an object at infinity to a short distance object.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a cross-sectional view at a wide angle end and in focus at infinity according to Numerical Embodiment 1.

FIG. 2 is an aberration diagram at the wide angle end and in focus at 2.5 m according to Numerical Embodiment 1.

FIG. 3 is an aberration diagram at a telephoto end and in focus at 3.5 m according to Numerical Embodiment 1.

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FIG. 4 is an aberration diagram at the telephoto end and in focus at infinity according to Numerical Embodiment 1.

FIG. 5 is an aberration diagram at the telephoto end and in focus at 0.85 m according to Numerical Embodiment 1.

FIG. 6 is a cross-sectional view at the wide angle end and in focus at infinity according to Numerical Embodiment 2.

FIG. 7 is an aberration diagram at the wide angle end and in focus at 2.5 m according to Numerical Embodiment 2.

FIG. 8 is an aberration diagram at the telephoto end and in focus at 3.5 m according to Numerical Embodiment 2.

FIG. 9 is an aberration diagram at the telephoto end and in focus at infinity according to Numerical Embodiment 2.

FIG. 10 is an aberration diagram at the telephoto end and in focus at 0.85 m according to Numerical Embodiment 2.

FIG. 11 is a cross-sectional view at the wide angle end and in focus at infinity according to Numerical Embodiment 3.

FIG. 12 is an aberration diagram at the wide angle end and in focus at 3.5 m according to Numerical Embodiment 3.

FIG. 13 is an aberration diagram at the telephoto end and in focus at 3.5 m according to Numerical Embodiment 3.

FIG. 14 is an aberration diagram at the telephoto end and in focus at infinity according to Numerical Embodiment 3.

FIG. 15 is an aberration diagram at the telephoto end and in focus at 0.6 m according to Numerical Embodiment 3.

FIG. 16 is a schematic diagram illustrating dichroic achromatism and remaining secondary spectrum of a positive lens unit.

FIG. 17 is a schematic diagram of distribution of an Abbe constant v and a partial dispersion ratio θ of optical materials.

DESCRIPTION OF THE EMBODIMENTS

A zoom lens according to the present invention is described in detail referring to the attached drawings.

The zoom lens according to the present invention includes, in order from an object side to an image side, a first lens unit having a positive refractive power, a second lens unit having a negative refractive power which moves during zooming, a third lens unit which moves in an optical axis direction for correcting an image plane position, a stop, and a fourth lens unit having a positive refractive power for image formation. The first lens unit includes a first lens subunit having a negative refractive power which does not move, a second lens subunit having a positive refractive power which moves during focus adjustment, and a third lens subunit having a positive refractive power which does not move. The first lens subunit includes only a lens having a negative refractive power, and the second lens subunit includes at least one positive lens and at least one negative lens.

The zoom lens of the present invention satisfies the following conditional expressions:

$$9 \times 10^6 < v_{11a}^3 \times (v_{12ap} - v_{12an}) < 45 \times 10^6 \quad (1),$$

$$1.8 < \phi_{11}/\phi_{12} < 7.0 \quad (2), \text{ and}$$

$$0.5 < \phi_{11}/\phi_1 < 1.0 \quad (3),$$

where ϕ_{11} represents a refractive power of the first lens subunit, ϕ_{12} represents a refractive power of the second lens subunit, ϕ_1 represents a refractive power of the first lens unit, v_{11a} represents an average value of Abbe constants of the first lens subunit, v_{12ap} represents an average value of Abbe constants of lenses having positive refractive powers of the second lens subunit, and v_{12an} represents an average value of Abbe constants of lenses having negative refractive powers of the second lens subunit.

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It is preferred that, the zoom lens satisfy the following conditional expression:

$$0.020 < \theta_{11a} \times (\theta_{12an} - \theta_{12ap}) < 0.046 \quad (4),$$

where θ_{11a} represents an average value of partial dispersion ratios of materials of lenses included in the first lens subunit, θ_{12ap} represents an average value of partial dispersion ratios of materials of lenses having positive refractive powers included in the second lens subunit, and θ_{12an} represents an average value of partial dispersion ratios of materials of lenses having negative refractive powers included in the second lens subunit. Here, a partial dispersion ratio $\theta = (N_g - N_F) / (N_F - N_C)$ holds, where N_g represents a refractive index at g-line, N_F represents a refractive index at F-line and N_C represents a refractive power at C-line.

It is more preferred that, the zoom lens satisfy the following conditional expressions:

$$0.5 < v_{11a} / (v_{13ap} - v_{13an}) < 4.0 \quad (5), \text{ and}$$

$$0.6 < \phi_{13} / \phi_1 < 1.5 \quad (6),$$

where ϕ_{13} represents a refractive power of the third lens subunit, and v_{13a} represents an average value of Abbe constants of materials of lenses included in the third lens subunit.

In addition, the zoom lens satisfies the following conditional expression:

$$0.15 < |\phi_1 / \phi_2| < 0.30 \quad (7),$$

where ϕ_2 represents a refractive power of the second lens unit.

The conditional expressions (1) to (7) define conditions of the zoom lens configuration, dispersion characteristics of lens materials, and refractive powers thereof, so as to define conditions to achieve reductions in size and weight of the zoom lens, secondary spectrum correction of axial chromatic aberration at a telephoto end, and good optical performance with suppressed variation of performance over the entire focus range from an object at infinity to a short distance object.

An outline of secondary spectrum of axial chromatic aberration at the telephoto end is described with reference to FIGS. 16 and 17. FIG. 16 illustrates a schematic diagram concerning dichroic achromatism and remaining secondary spectrum of a positive lens unit. FIG. 17 shows a schematic diagram of distribution of Abbe constants v and partial dispersion ratios θ of existing optical materials. Here, when a refractive index for g-line is represented by N_g , a refractive index for F-line is represented by N_F , a refractive index for d-line is represented by N_d , and a refractive index for C-line is represented by N_C , the Abbe constant v and the partial dispersion ratio θ satisfy the following expressions (8) and (9), respectively.

$$v = (N_d - 1) / (N_F - N_C) \quad (8)$$

$$\theta = (N_g - N_F) / (N_F - N_C) \quad (9)$$

As shown in FIG. 17, the existing optical material is distributed in a region having a narrow partial dispersion ratio θ with respect to the Abbe constant v , and there is a tendency that the partial dispersion ratio θ increases as the Abbe constant v decreases.

A correction condition of chromatic aberration of a thin lens system which has a predetermined refractive power ϕ and includes two lenses 1 and 2 having refractive powers ϕ_1 and ϕ_2 and Abbe constants v_1 and v_2 , respectively, is expressed by the following expression.

$$\phi_1 / v_1 + \phi_2 / v_2 = 0 \quad (10)$$

Here, ϕ is expressed as follows.

$$\phi = \phi_1 + \phi_2 \quad (11)$$

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When the expression (10) is satisfied, an image position is identical between the C-line and the F-line.

In this case, the refractive powers ϕ_1 and ϕ_2 are expressed by the following expressions.

$$\phi_1 = \phi \times v_1 / (v_1 - v_2) \quad (12)$$

$$\phi_2 = -\phi \times v_2 / (v_1 - v_2) \quad (13)$$

In FIG. 16, as to the achromatism for the positive lens unit, a material having a large Abbe constant v_1 is used for the positive lens 1, and a material having a small Abbe constant v_2 is used for the negative lens 2. Therefore, the positive lens 1 has a small partial dispersion ratio θ_1 , and the negative lens 2 has a large partial dispersion ratio θ_2 as shown in FIG. 17. Thus, when the chromatic aberration is corrected at the F-line and the C-line, the image point at the g-line is shifted to the image side. This deviation amount defined as a secondary spectrum amount Δ is expressed by the following expression.

$$\Delta = -(1/\phi) \times (\theta_1 - \theta_2) / (v_1 - v_2) \quad (14)$$

The secondary spectrum amount Δ of the entire lens system is expressed by the following expression:

$$\Delta = \Delta_{11} \times \beta_{12}^2 \times \beta_{13}^2 \times \beta_Z^2 + \Delta_{12} \times (1 - \beta_{12}) \times \beta_{13}^2 \times \beta_Z^2 + \Delta_{13} \times (1 - \beta_{13}) \times \beta_Z^2 + \Delta_Z \times (1 - \beta_Z) \quad (15)$$

where Δ_{11} , Δ_{12} , Δ_{13} , and Δ_Z represent the secondary spectrum amounts of the first lens subunit, the second lens subunit, the third lens subunit, and the lens unit after the zooming system, respectively, and β_{12} , β_{13} , and β_Z represent imaging magnification of the second lens subunit, the third lens subunit, and the lens unit after the zooming system, respectively.

The secondary spectrum amount Δ becomes significant in the first lens subunit to the third lens subunit in which an axial marginal light beam passes through at a high position on the telephoto side. Therefore, the secondary spectrum amount Δ of the axial chromatic aberration may be reduced on the telephoto side by suppressing the sum of the secondary spectrum amounts Δ_{11} , Δ_{12} , and Δ_{13} of the axial chromatic aberration generated in the first lens subunit to the third lens subunit.

Next, a variation of performance over the entire focus range from an object at infinity to a short distance object is described. Here, Δ_{inf} represents a secondary spectrum amount at an object at infinity, Δ_{mod} represents a secondary spectrum amount of a short distance object that is photographable. In addition, Δ_{11inf} and Δ_{12inf} represent secondary spectrum amounts of the first lens subunit and the second lens subunit at an object at infinity, and Δ_{11mod} and Δ_{12mod} represent secondary spectrum amounts of the first lens subunit and the second lens subunit at a short distance object. In addition, β_{12inf} represents an imaging magnification of the second lens subunit at an object at infinity, and β_{12mod} represents an imaging magnification of the second lens subunit at a shortest distance object. Because the second lens subunit is a focus lens unit, a position on the optical axis of an object point of the third lens subunit does not change regardless of the object distance. Therefore, Δ_{13} , Δ_Z , β_{13} , and β_Z do not change depending on the object distance. In this case, a variation amount Δ_{obj} of the secondary spectrum of axial chromatic aberration of a short distance object with respect to an object at infinity is expressed by the following expression derived from the expression (13).

$$\Delta_{obj} = \Delta_{mod} - \Delta_{inf} = \{ (\Delta_{11mod} \times \beta_{12mod}^2 - \Delta_{11inf} \times \beta_{12inf}^2) - (\Delta_{12mod} \times \beta_{12mod} - \Delta_{12inf} \times \beta_{12inf}) \times \beta_{13}^2 \times \beta_Z^2 \} \quad (16)$$

By suppressing an absolute value in { } of the expression (16), it is possible to suppress the variation of axial chromatic

aberration performance over the entire focus range from an object at infinity to a short distance object. By defining conditions of the zoom lens configuration, dispersion characteristics of lens materials, and refractive powers thereof using the conditional expressions (1) to (7), it is possible to suppress the absolute value in { } of the expression (16).

The conditional expression (1) defines a relationship between Abbe constants v of the positive lens and the negative lens. When the upper limit condition of the conditional expression (1) is not satisfied, it becomes difficult to maintain performance balance between axial chromatic aberration and lateral chromatic aberration over the entire zoom range. In addition, when the lower limit condition of the conditional expression (1) is not satisfied, it becomes difficult to suppress the variation of axial chromatic aberration over the entire focus range. It is more preferred that the conditional expression (1) define the following range.

$$9 \times 10^6 < v_{11} a^3 (v_{12ap} - v_{12an}) < 30 \times 10^6 \quad (1a)$$

The conditional expression (2) defines a relationship between the refractive powers of the first lens subunit and the second lens subunit. When the refractive power ϕ_{11} of the first lens subunit increases to dissatisfy the upper limit condition of the conditional expression (2), the variation of $\Delta 11_{inf}$ to $\Delta 11_{mod}$ in the expression (16) increases so that it becomes difficult to suppress the variation of axial chromatic aberration performance over the entire focus range.

In addition, when the refractive power ϕ_{12} of the second lens subunit decreases to dissatisfy the upper limit condition of the conditional expression (2), a movement amount of the second lens subunit due to focusing increases so that it becomes difficult to achieve reductions in size and weight. In addition, when the refractive power ϕ_{11} of the first lens subunit decreases to dissatisfy the lower limit condition of the conditional expression (2), a lens outer diameter of the first lens unit increases so that it becomes difficult to achieve reductions in size and weight. Further, it becomes difficult to achieve a wider angle of field of the zoom lens, or to secure a lens interval between the first lens unit and the second lens unit. When the refractive power ϕ_{12} of the second lens subunit increases to dissatisfy the lower limit condition of the conditional expression (2), a variation from $\Delta 12_{inf}$ to $\Delta 12_{mod}$ and a variation from $\beta 12_{inf}$ to $\beta 12_{mod}$ in the expression (16) increase so that it becomes difficult to suppress the variation of axial chromatic aberration performance over the entire focus range. It is more preferred that the conditional expression (2) define the following range.

$$1.8 < \phi_{11} / \phi_{12} < 7.0 \quad (2a)$$

The conditional expression (3) defines a relationship between the refractive powers of the first lens subunit and the entire first lens unit. When the refractive power ϕ_{11} of the first lens subunit increases to dissatisfy the upper limit condition of the conditional expression (3), the variation of $\Delta 11_{inf}$ to $\Delta 11_{mod}$ in the expression (16) increases so that it becomes difficult to suppress the variation of axial chromatic aberration performance over the entire focus range. When the refractive power ϕ_1 of the first lens unit decreases to dissatisfy the upper limit condition of the conditional expression (3), the lens outer diameter of the first lens unit increases so that it becomes difficult to achieve reductions in size and weight. Further, it becomes difficult to achieve a wider angle of field of the zoom lens. In addition, when the refractive power ϕ_{11} of the first lens subunit decreases to dissatisfy the lower limit condition of the conditional expression (3), the lens outer diameter of the first lens unit increases so that it becomes difficult to achieve reductions in size and weight. Further, it

becomes difficult to achieve a wider angle of field of the zoom lens, or to secure the lens interval between the first lens unit and the second lens unit. When the refractive power ϕ_1 of the first lens unit increases to dissatisfy the lower limit condition of the conditional expression (3), it becomes difficult to maintain good optical performance over the entire zoom range and the entire focus range. It is more preferred that the conditional expression (3) define the following range.

$$0.5 < |\phi_{11} / \phi_1| < 1.0 \quad (3a)$$

The conditional expression (4) defines a relationship between partial dispersion ratios θ of the positive lens and the negative lens. When the upper limit condition of the conditional expression (4) is not satisfied, it becomes difficult to correct secondary spectrum of axial chromatic aberration at the telephoto end. In addition, when the lower limit condition of the conditional expression (4) is not satisfied, the secondary spectrum correction of the axial chromatic aberration at the telephoto end becomes excessive so that it becomes difficult to maintain performance balance between axial chromatic aberration and lateral chromatic aberration over the entire zoom range. It is more preferred that the conditional expression (4) define the following range.

$$0.030 < \theta_{11a} (\theta_{12an} - \theta_{12ap}) < 0.045 \quad (4a)$$

The conditional expression (5) defines a relationship between Abbe constants of the first lens subunit and the third lens subunit. By satisfying the conditional expression (5), it is possible to achieve appropriate performance balance between axial chromatic aberration and lateral chromatic aberration over the entire zoom range and the entire focus range. It is more preferred that the conditional expression (5) define the following range.

$$0.6 < v_{11a} (v_{13ap} - v_{13an}) < 3.5 \quad (5a)$$

The conditional expression (6) defines a relationship between the refractive powers of the third lens subunit and the first lens unit. When the refractive power ϕ_{13} of the third lens subunit increases to dissatisfy the upper limit condition of the conditional expression (6), it becomes difficult to achieve good optical performance at the telephoto end. When the refractive power of the first lens unit decreases to dissatisfy the upper limit condition of the conditional expression (6), the lens outer diameter of the first lens unit increases so that it becomes difficult to achieve reductions in size and weight. Further, it becomes difficult to achieve a wider angle of field of the zoom lens. In addition, when the refractive power of the third lens subunit decreases to dissatisfy the lower limit condition of the conditional expression (6), the lens outer diameter of the first lens unit increases so that it becomes difficult to achieve reductions in size and weight. Further, it becomes difficult to secure the lens interval between the first lens unit and the second lens unit. When the refractive power ϕ_1 of the first lens unit increases to dissatisfy the lower limit condition of the conditional expression (6), it becomes difficult to maintain good optical performance over the entire zoom range and the entire focus range. It is more preferred that the conditional expression (6) define the following range.

$$0.7 < \phi_{13} / \phi_1 < 1.3 \quad (6a)$$

The conditional expression (7) defines a relationship of refractive powers of the first lens unit and the second lens unit, and refractive powers at a wide angle end and at the telephoto end in order to achieve a wider angle of field, a higher zoom ratio, and reductions in size and weight.

When the refractive power ϕ_1 decreases to dissatisfy the lower limit condition of the conditional expression (7), it

becomes difficult to achieve a wider angle of field and reduction in size and weight. In addition, when the refractive power $\phi 2$ increases to dissatisfy the lower limit condition of the conditional expression (7), it becomes difficult to achieve good optical performance over the entire zoom range. When the refractive power $\phi 1$ increases to dissatisfy the upper limit condition of the conditional expression (7), it becomes difficult to maintain good optical performance over the entire zoom range and the entire focus range. In addition, when the refractive power $\phi 2$ decreases to dissatisfy the upper limit condition of the conditional expression (7), it becomes difficult to secure a zoom ratio and to achieve a small size and light weight. It is more preferred that the conditional expression (7) define the following range.

$$0.18 < |\phi 1 / \phi 2| < 0.30 \tag{7a}$$

In addition, some of the conditional expressions (1) to (7) use the average value for defining. When a lens having an extremely small refractive power like a flat glass plate is included, the range of the conditional expression may be exceeded. Therefore, it is supposed that using any number of lenses having an extremely small refractive power is included in the present invention.

Embodiment 1

FIG. 1 illustrates a lens cross-sectional view of a zoom lens at the wide angle end and in focus at an object distance of infinity according to Embodiment 1 of the present invention.

The zoom lens of this embodiment includes, in order from the object side to the image side, a front lens unit having a positive refractive power as a first lens unit F, a variator having a negative refractive power as a second lens unit V that moves for zooming, a compensator having a negative refractive power as a third lens unit C, a stop SP, and a fixed relay lens unit having a positive refractive power and an image forming action as a fourth lens unit R.

The first lens unit F includes, in order from the object side to the image side, the first lens subunit that does not move for focusing, the second lens subunit that moves in an optical axis direction during focusing, and the third lens subunit that does not move for focusing. The second lens unit V monotonously moves on the optical axis to the image plane side to zoom from the wide angle end to the telephoto end. The third lens unit C moves non-linearly on the optical axis in order to correct image plane variation due to zooming. The variator V and the compensator C construct a zoom optical system. A glass block P illustrated in FIG. 1 is a color separation prism, an optical filter, or the like. An image plane I corresponds to an image plane of an image pickup element of an image pickup apparatus connected to the zoom lens of the present invention, and receives light from the zoom lens.

FIG. 2 illustrates an aberration diagram in focus at a distance of 2.5 m from a vertex of a first surface of the lens at the wide angle end of Embodiment 1. FIG. 3 illustrates an aberration diagram in focus at an object distance of 3.5 m at the telephoto end. FIG. 4 illustrates an aberration diagram in focus at an object distance of infinity at the telephoto end.

FIG. 5 illustrates an aberration diagram in focus at a minimum object optical distance of 0.85 m at the telephoto end.

The aberration diagram illustrates, in order from the left to the right, spherical aberration, field curvature, distortion, and lateral chromatic aberration. A unit of the horizontal axis in each aberration diagram is mm for the spherical aberration, the field curvature, and the lateral chromatic aberration, and is % for the distortion. For the spherical aberration, the distortion, and the lateral chromatic aberration, a solid line indicates an e-line, a double-dotted dashed line indicates a g-line, and a dotted dashed line indicates a C-line. For the field curvature, a solid line indicates a sagittal section of the e-line, a dotted line indicates a meridional section of the e-line, a dotted dashed line indicates a sagittal section of the g-line, and a double-dotted dashed line indicates a value in the meridional section of the g-line. The same is true in the following embodiments.

In the following, Numerical Embodiment corresponding to this embodiment is described.

An aspherical shape is expressed by the following expression:

$$X = \frac{(1/R)H^2}{1 + \sqrt{1 - (1 + K)(H/R)^2}} + A3 \cdot H^3 + A4 \cdot H^4 + A5 \cdot H^5 + A6 \cdot H^6 + A7 \cdot H^7 + A8 \cdot H^8 + A9 \cdot H^9 + A10 \cdot H^{10} + A11 \cdot H^{11} + A12 \cdot H^{12}$$

where A3 to A12 represent aspheric coefficients, and the aspherical shape is expressed by a displacement x in the optical axis direction with respect to a surface vertex at a position having a height H from the optical axis. Here, R represents a paraxial radius of curvature and K represents a conic constant.

The first lens unit of this embodiment corresponds to the first surface to the sixteenth surface, and includes the first lens subunit from the first surface to the fourth surface, the second lens subunit from the fifth surface to the tenth surface, and the third lens subunit from the eleventh surface to the sixteenth surface.

Table 1 shows variation amounts of imaging positions in focus at a closest distance object and corresponding values of the conditional expressions with respect to the imaging position in focus at an object distance of infinity, for the image position of a light beam close to the optical axis of the g-line at the telephoto end of this embodiment. The variation amount is positive in the direction toward the image plane along the optical axis.

The zoom lens of this embodiment has a feature in that the expressions (1) and (5) are close to the lower limits. Numerical Embodiment 1 satisfies all the conditional expressions. According to the present invention, it is possible to achieve good optical performance with suppressed variation of performance over the entire focus range from an object at infinity to a short distance object with the simple structure of the first lens unit.

Numerical Embodiment 1

Unit mm						
Surface data						
Surface number	r	d	nd	vd	θgF	Effective diameter

-continued

Unit mm						
1	326.535	3.12	1.69680	55.5	0.543	102.07
2	82.442	19.62				89.85
3	-169.843	2.90	1.64000	60.1	0.537	89.62
4	457.137	10.36				87.30
5	-1260.023	8.66	1.62041	60.3	0.543	85.61
6	-118.623	0.15				85.45
7	542.881	2.60	1.89676	23.0	0.611	79.70
8	120.218	0.06				78.25
9	119.37	9.87	1.49700	81.5	0.537	78.28
10	-458.06	11.23				78.19
11	162.023	9.71	1.43387	95.1	0.537	77.50
12	-211.577	0.15				77.67
13	127.700	10.54	1.59522	67.7	0.544	77.80
14	-245.288	0.15				77.48
15	51.206	6.88	1.59522	67.7	0.544	68.01
16	82.430	(Variable)				66.96
17	223.104	1.00	1.88300	40.8	0.567	28.44
18	18.464	6.08				23.50
19	-73.560	6.21	1.92286	18.9	0.650	22.81
20	-17.626	0.75	1.88300	40.8	0.567	22.21
21	284.333	0.19				21.05
22	27.750	4.47	1.56732	42.8	0.573	20.35
23	-429.295	2.31				19.04
24	-25.489	0.75	1.88300	40.8	0.567	18.43
25	-144.116	(Variable)				18.45
26	-29.430	0.75	1.81600	46.6	0.557	20.22
27	61.570	3.77	1.80810	22.8	0.631	21.85
28	-181.636	(Variable)				22.98
29 (Stop)	0.000	1.30				27.09
30	827.779	5.35	1.67003	47.2	0.563	28.18
31	-34.493	0.14				29.04
32	60.461	4.63	1.51823	58.9	0.546	29.58
33	-139.516	0.20				29.37
34	110.651	6.14	1.48749	70.2	0.530	28.85
35	-34.259	1.15	1.88300	40.8	0.567	28.27
36	586.479	(Variable)				28.21
37	34.309	7.35	1.51823	58.9	0.546	28.91
38	-49.152	1.00				28.29
39	-172.357	1.00	1.88300	40.8	0.567	26.02
40	26.486	4.48	1.48749	70.2	0.530	24.43
41	152.332	0.50				24.08
42	117.611	6.70	1.48749	70.2	0.530	23.95
43	-19.443	1.00	1.88300	40.8	0.567	23.53
44	-38.198	1.18				24.04
45	51.241	3.38	1.48749	70.2	0.530	22.82
46	-624.228	4.50				22.15
47	0.000	33.00	1.60859	46.4	0.566	40.00
48	0.000	13.2	1.51633	64.2	0.535	40.00
49	0.000					40.00

Aspherical surface data			
Seventeenth surface			
K = -1.42317e+003	A4 = 3.79405e-005	A6 = -3.60242e-009	A8 = -2.54644e-010
A10 = 2.12348e-012	A12 = -4.16310e-015		
A3 = 9.41919e-006	A5 = -2.00743e-006	A7 = 4.85928e-009	A9 = -2.60328e-011
A11 = 4.24769e-014			
Twenty-second surface			
K = 1.15980e+000	A4 = -1.49547e-005	A6 = 6.23650e-008	A8 = -1.26337e-009
A10 = -1.91096e-012	A12 = 7.54862e-014		
A3 = -4.26107e-005	A5 = -7.85671e-007	A7 = -2.81272e-009	A9 = 2.92291e-010
A11 = -1.87611e-012			

Various data			
Zoom ratio 20.51			
	Wide angle	Intermediate	Telephoto
Focal length	6.80	41.21	139.50
F-number	1.97	1.95	2.69
Angle of field	38.97	7.60	2.26
Image height	5.50	5.50	5.50
Total lens length	325.99	325.99	325.99
BF	8.65	8.65	8.65
d16	2.03	42.89	53.18

-continued

Unit mm					
d25		56.69	9.85	9.08	
d28		4.85	10.81	1.30	
d36		35.30	35.30	35.30	
d49		8.65	8.65	8.65	
Incident pupil position		63.08	193.55	440.88	
Exit pupil position		1107.27	1107.27	1107.27	
Front principal point position		69.93	236.31	598.09	
Rear principal point position		1.85	-32.56	-130.84	
Zoom lens unit data					
Unit	First surface	Focal length	Lens structure length	Front principal point position	Rear principal point position
1	1	55.34	95.98	62.95	17.36
2	17	-13.32	21.76	4.22	-9.02
3	26	-43.25	4.52	-0.48	-3.00
4	29	37.95	18.92	1.73	-10.09
5	37	53.71	77.30	9.13	-45.19

Embodiment 2

FIG. 6 illustrates a lens cross-sectional view of the zoom lens at the wide angle end in focus at an object distance of infinity according to Embodiment 2 of the present invention.

The zoom lens of this embodiment includes, in order from the object side to the image side, a front lens unit having a positive refractive power as a first lens unit F, a variator having a negative refractive power as a second lens unit V that moves during zooming, a compensator having a negative refractive power as a third lens unit C, a stop SP, and a fixed relay lens unit having a positive refractive power and an image forming action as a fourth lens unit R.

The first lens unit F includes, in order from the object side to the image side, the first lens subunit that does not move for focusing, the second lens subunit that moves in an optical axis direction during focusing, and the third lens subunit that does not move for focusing. The second lens unit V monotonously moves on the optical axis to the image plane side to zoom from the wide angle end to the telephoto end. The third lens unit C moves non-linearly on the optical axis in order to correct image plane variation due to zooming. The variator V and the compensator C construct a zoom optical system. A glass block P illustrated in FIG. 1 is a color separation prism, an optical filter, or the like. An image plane I corresponds to an image plane of an image pickup element of an image pickup apparatus connected to the zoom lens of the present invention, and receives light from the zoom lens.

FIG. 7 illustrates an aberration diagram in focus at a distance of 2.5 m from a vertex of a first surface of the lens at the wide angle end of Embodiment 2. FIG. 8 illustrates an aber-

ration diagram in focus at an object distance of 3.5 m at the telephoto end. FIG. 9 illustrates an aberration diagram in focus at an object distance of infinity at the telephoto end. FIG. 10 illustrates an aberration diagram in focus at a minimum object optical distance of 0.85 m at the telephoto end.

The first lens unit of this embodiment corresponds to the first surface to the eighteenth surface, and includes the first lens subunit from the first surface to the fourth surface, the second lens subunit from the fifth surface to the tenth surface, and the third lens subunit from the eleventh surface to the eighteenth surface.

Table 1 shows variation amounts of image positions in focus at a close distance and corresponding values of the conditional expressions with respect to the image position in focus at an object distance of infinity, for the image position of a light beam close to the optical axis of the g-line at the telephoto end of this embodiment. The variation amount is positive in the direction toward the image plane along the optical axis.

The zoom lens of this embodiment has a feature in that the expressions (1), (5), and (6) are close to the upper limits, and the expressions (2), (3), (4), and (7) are close to the lower limits.

Numerical Embodiment 2 satisfies all the conditional expressions. According to the present invention, it is possible to achieve good optical performance with suppressed variation of performance over the entire focus range from an object at infinity to a short distance object with the simple structure of the first lens unit.

Numerical Embodiment 2

Unit mm						
Surface data						
Surface number	r	d	nd	vd	θ_{gF}	Effective diameter
1	635.963	3.12	1.64000	60.1	0.537	106.03
2	132.576	13.35				97.52
3	-304.897	2.90	1.49700	81.5	0.537	97.40
4	168.803	1.92				91.87
5	184.712	9.75	1.43387	95.1	0.537	91.42

-continued

Unit mm						
6	-384.210	0.15				90.90
7	252.194	2.60	1.84666	23.8	0.603	86.24
8	103.580	1.26				82.26
9	118.656	12.50	1.43387	95.1	0.537	82.24
10	-231.352	17.86				82.11
11	113.023	12.49	1.59522	67.7	0.544	76.80
12	-163.251	0.45				76.70
13	-161.806	2.37	1.77250	49.6	0.552	76.60
14	-399.495	0.15				76.80
15	103.772	9.10	1.49700	81.5	0.537	75.88
16	-1123.478	0.15				75.37
17	61.402	6.68	1.59522	67.7	0.544	68.07
18	104.593	(Variable)				66.45
19	211.537	1.00	1.88300	40.8	0.567	25.00
20	13.555	6.40				19.91
21	-48.675	5.92	1.92286	18.9	0.650	19.59
22	-16.822	0.75	1.88300	40.8	0.567	19.75
23	248.618	0.19				19.78
24	26.790	5.69	1.56732	42.8	0.573	19.94
25	-40.427	0.83				19.43
26	-35.916	0.75	1.88300	40.8	0.567	19.26
27	1266.739	(Variable)				19.54
28	-27.875	0.75	1.81600	46.6	0.557	20.24
29	64.230	3.80	1.80810	22.8	0.631	21.98
30	-137.856	(Variable)				23.12
31	0.000	1.30				27.36
32	-126.052	4.06	1.67003	47.2	0.563	27.77
33	-31.943	0.14				28.55
34	43.506	5.62	1.51823	58.9	0.546	30.11
35	-122.349	0.20				29.92
36	82.040	6.03	1.48749	70.2	0.530	29.26
37	-40.840	1.15	1.88300	40.8	0.567	28.62
38	177.690	(Variable)				28.31
39	37.769	6.86	1.51823	58.9	0.546	28.60
40	-50.856	1.00				28.04
41	-221.775	1.00	1.88300	40.8	0.567	25.98
42	28.189	4.40	1.48749	70.2	0.530	24.56
43	183.482	0.50				24.50
44	78.324	6.82	1.48749	70.2	0.530	24.55
45	-21.482	1.00	1.88300	40.8	0.567	24.40
46	-56.126	1.18				25.16
47	41.302	4.22	1.48749	70.2	0.530	25.26
48	-337.860	4.50				24.88
49	0.000	33.00	1.60859	46.4	0.566	40.00
50	0.000	13.20	1.51633	64.2	0.535	40.00
51	0.000					40.00
Aspherical surface data						
Nineteenth surface						
K = -1.42317e+003	A4 = 3.71629e-005	A6 = 1.91864e-009	A8 = -3.96049e-010			
A10 = 3.84440e-012	A12 = -5.88236e-015					
A3 = 1.71450e-005	A5 = -2.01987e-006	A7 = 2.03343e-009	A9 = -3.39056e-012			
A11 = -6.48408e-014						
Twenty-fourth surface						
K = 1.15980e+000	A4 = -6.20631e-006	A6 = 5.61707e-008	A8 = -1.23147e-009			
A10 = 3.00740e-012	A12 = 6.72120e-014					
A3 = -4.34636e-005	A5 = -1.05401e-006	A7 = 2.67413e-009	A9 = 1.75172e-010			
A11 = -1.68464e-012						
Various data						
Zoom ratio 20.51						
	Wide angle	Intermediate	Telephoto			
Focal length	8.00	48.49	164.11			
F-number	1.97	1.95	2.75			
Angle of field	34.51	6.47	1.92			
Image height	5.50	5.50	5.50			
Total lens length	323.23	323.23	323.23			
BF	8.57	8.57	8.57			
d18	2.28	43.15	53.44			
d27	53.20	6.37	5.59			
d30	4.85	10.81	1.30			
d38	35.30	35.30	35.30			

-continued

Unit mm					
d51		8.57	8.57	8.57	
Incident pupil position		74.85	255.58	599.66	
Exit pupil position		1200.00	1200.00	1200.00	
Front principal point position		82.90	306.04	786.38	
Rear principal point position		0.57	-39.92	-155.55	

Zoom lens unit data					
Unit	First surface	Focal length	Lens structure length	Front principal point position	Rear principal point position
1	1	65.11	96.79	63.17	5.27
2	19	-13.32	21.52	1.64	-12.67
3	28	-43.25	4.55	-0.64	-3.19
4	31	37.95	18.49	1.26	-10.20
5	39	53.32	77.68	8.90	-45.46

Embodiment 3

FIG. 11 illustrates a lens cross-sectional view of a zoom lens at the wide angle end in focus at infinity according to Embodiment 3 of the present invention.

The zoom lens of this embodiment includes, in order from the object side to the image side, a front lens unit having a positive refractive power as a first lens unit F, a variator having a negative refractive power as a second lens unit V that moves during zooming, a compensator having a positive refractive power as a third lens unit C, a stop SP, and a fixed relay lens unit having a positive refractive power and an image forming action as a fourth lens unit R.

The first lens unit F includes, in order from the object side to the image side, the first lens subunit that does not move for focusing, the second lens subunit that moves in an optical axis direction during focusing, and the third lens subunit that does not move for focusing. The second lens unit V monotonously moves on the optical axis to the image plane side to zoom from the wide angle end to the telephoto end. The third lens unit C moves non-linearly on the optical axis in order to correct image plane variation due to zooming. The variator V and the compensator C construct a zoom optical system. A glass block P illustrated in FIG. 1 is a color separation prism, an optical filter, or the like. An image plane I corresponds to an image plane of an image pickup element of an image pickup apparatus connected to the zoom lens of the present invention, and receives light from the zoom lens.

FIG. 12 illustrates an aberration diagram in focus at a distance of 3.5 m from a vertex of a first surface of the lens at

the wide angle end of Embodiment 3. FIG. 13 illustrates an aberration diagram in focus at an object distance of 3.5 m at the telephoto end. FIG. 14 illustrates an aberration diagram in focus at an object distance of infinity at the telephoto end. FIG. 15 illustrates an aberration diagram in focus at a minimum object optical distance of 0.6 m at the telephoto end.

The first lens unit of this embodiment corresponds to the first surface to the fifteenth surface, and includes the first lens subunit from the first surface to the fourth surface, the second lens subunit from the fifth surface to the seventh surface, and the third lens subunit from the eighth surface to the fifteenth surface.

Table 1 shows variation amounts of image positions in focus at a close distance and corresponding values of the conditional expressions with respect to the image position in focus at an object distance of infinity, for the image position of a light beam close to the optical axis of the g-line at the telephoto end of this embodiment. The variation amount is positive in the direction toward the image plane along the optical axis.

This embodiment has a feature in that the expressions (2), (3), (4), (5), and (7) are close to the upper limits.

Numerical Embodiment 3 satisfies all the conditional expressions. According to the present invention, it is possible to achieve good optical performance with suppressed variation of performance over the entire focus range from an object at infinity to a short distance object with the simple structure of the first lens unit.

Numerical Embodiment 3

Unit mm						
Surface data						
Surface number	r	d	nd	vd	θgF	Effective diameter
1	1827.374	5.28	1.62041	60.3	0.543	202.67
2	151.905	40.99				172.12
3	-336.820	4.34	1.59522	67.7	0.544	168.87
4	333.950	18.86				161.03
5	-576.133	4.14	1.89676	23.0	0.611	160.33
6	8486.577	26.34	1.43875	94.9	0.534	160.59
7	-152.838	42.91				160.72
8	498.689	21.62	1.43387	95.1	0.537	140.91
9	-206.241	0.20				141.89
10	176.739	4.24	1.80000	29.8	0.602	142.92

-continued

Unit mm						
11	126.249	0.15				139.24
12	124.137	30.61	1.43387	95.1	0.537	139.51
13	-676.188	0.15				138.69
14	181.430	13.56	1.59522	67.7	0.544	133.68
15	1495.754	(Variable)				132.59
16	-339.870	2.37	1.77250	49.5	0.552	57.57
17	38.827	2.25				48.15
18	39.734	12.50	1.80810	22.8	0.631	47.61
19	-119.206	1.42	1.75500	52.3	0.548	48.01
20	56.883	10.46				41.63
21	-68.034	1.42	1.88300	40.8	0.567	37.59
22	206.909	(Variable)				38.50
23	63.779	11.89	1.60311	60.6	0.541	54.14
24	-127.664	0.15				54.09
25	477.469	4.78	1.45600	90.3	0.534	53.39
26	-177.651	0.62				53.03
27	-312.583	1.88	1.80518	25.4	0.616	52.41
28	66.849	7.00	1.49700	81.5	0.537	51.23
29	1292.504	0.25				51.22
30	70.254	9.51	1.60311	60.6	0.541	51.28
31	-122.032	(Variable)				50.77
32	0.000	2.67				27.52
33	-86.165	1.50	1.75500	52.3	0.548	26.47
34	17.966	4.68	1.80810	22.8	0.631	24.93
35	42.830	5.00				24.57
36	-54.029	1.50	1.77250	49.6	0.552	24.61
37	44.067	5.40	1.60342	38.0	0.584	25.65
38	-28.982	1.98				25.79
39	-23.954	1.60	1.81600	46.6	0.557	25.67
40	77.096	5.88	1.59551	39.2	0.580	28.99
41	-29.020	18.76				29.33
42	-83.163	7.53	1.53172	48.8	0.563	36.46
43	-39.171	4.18				38.20
44	195.219	2.00	1.88300	40.8	0.567	38.28
45	35.281	9.48	1.49700	81.5	0.537	37.70
46	-98.039	0.19				38.18
47	97.193	9.59	1.48749	70.2	0.530	38.74
48	-37.015	2.00	1.72151	29.2	0.605	38.65
49	-137.205	0.20				39.45
50	136.692	8.41	1.48749	70.2	0.530	39.50
51	-45.320	13.04				39.29
52	0.000	33.00	1.60859	46.4	0.566	50.00
53	0.000	13.20	1.51633	64.2	0.535	50.00
54	0.000					50.00
Aspherical surface data						
First surface						
K = -8.69519e+001	A4 = -3.47108e-010	A6 = -4.74203e-012	A8 = -4.20690e-014			
A10 = 7.94625e-018	A12 = 3.19482e-022					
A3 = 1.20625e-007	A5 = 9.32151e-011	A7 = 1.52457e-012	A9 = 1.01796e-016			
A11 = -9.42635e-020						
Sixteenth surface						
K = -2.07514e+002	A4 = 4.08573e-007	A6 = 2.74421e-010	A8 = 1.19778e-013			
A10 = 5.67687e-018	A12 = -8.47261e-018					
A3 = -1.27957e-006	A5 = -4.00784e-008	A7 = 1.23492e-010	A9 = -3.03665e-013			
A11 = 4.66186e-016						
Twenty-fourth surface						
K = -4.64153e+000	A4 = 1.49522e-006	A6 = 2.46711e-010	A8 = -2.17611e-012			
A10 = -9.19332e-016	A12 = -5.08645e-018					
A3 = -3.66022e-006	A5 = -3.67979e-008	A7 = 3.69369e-011	A9 = -1.19861e-014			
A11 = 2.34421e-016						
Thirty surface						
K = 6.53399e-001	A4 = -5.20729e-007	A6 = -1.73166e-009	A8 = -3.26956e-012			
A10 = 1.15604e-015	A12 = -2.48520e-018					
A3 = -4.48490e-006	A5 = -1.65097e-008	A7 = 4.44966e-011	A9 = 9.41486e-014			
A11 = 2.57580e-017						

-continued

Unit mm					
Various data					
Zoom ratio 29.98					
	Wide angle	Intermediate	Telephoto		
Focal length	6.00	26.17	179.90		
F-number	1.55	1.55	2.30		
Angle of field	42.51	11.87	1.75		
Image height	5.50	5.50	5.50		
Total lens length	614.53	614.53	614.53		
BF	11.83	11.83	11.83		
d15	2.66	79.66	120.52		
d22	166.35	76.63	1.18		
d31	2.00	14.71	49.30		
d54	11.83	11.83	11.83		
Incident pupil position	113.77	213.05	820.97		
Exit pupil position	92.11	92.11	92.11		
Front principal point position	120.22	247.76	1404.05		
Rear principal point position	5.83	-14.35	-168.08		
Zoom lens unit data					
Unit	First surface	Focal length	Lens structure length	Front principal point position	Rear principal point position
1	1	110.18	213.39	138.47	73.19
2	16	-28.30	30.44	13.76	-6.52
3	23	48.00	36.07	11.35	-14.52
4	32	28.36	151.80	43.41	10.31

TABLE 1

Variation amounts of image positions depending on object distance and corresponding values of conditional expressions			
Conditional expression number	Numerical Embodiment 1	Numerical Embodiment 2	Numerical Embodiment 3
(1)	9.3×10^6	25.3×10^6	18.8×10^6
(2)	2.92	2.10	5.86
(3)	0.67	0.565	0.87
(4)	0.038	0.035	0.042
(5)	0.752	3.114	1.139
(6)	0.901	0.978	0.85
(7)	0.24	0.21	0.26
Variation amount of image position	-0.073	-0.058	-0.135

While the present invention has been described with reference to exemplary embodiments, it is to be understood that the invention is not limited to the disclosed exemplary embodiments. The scope of the following claims is to be accorded the broadest interpretation so as to encompass all such modifications and equivalent structures and functions.

This application claims the benefit of Japanese Patent Application No. 2013-095318, filed Apr. 30, 2013, which is hereby incorporated by reference herein in its entirety.

What is claimed is:

1. A zoom lens, comprising, in order from an object side to an image side:

- a first lens unit having a positive refractive power;
- a second lens unit having a negative refractive power which moves during zooming;
- a third lens unit;
- a stop; and

a fourth lens unit having a positive refractive power, wherein the first lens unit includes, in order from the object side to the image side, a first lens subunit having a negative refractive power which does not move, a second lens subunit having a positive refractive power which moves during focusing, and a third lens subunit having a positive refractive power which does not move, wherein the first lens subunit is composed of one or more negative lenses, and the second lens subunit includes at least one positive lens and at least one negative lens, and wherein the following expression is satisfied:

$$9 \times 10^6 < v11a^3 \times (v12ap - v12an) < 45 \times 10^6,$$

where v11a represents an average value of Abbe constants of the first lens subunit, v12ap represents an average value of Abbe constants of the at least one positive lens of the second lens subunit, v12an represents an average value of Abbe constants of the at least one negative lens of the second lens subunit, and Abbe constant v is defined as,

$$v = (Nd - 1) / (NF - NC)$$

where NF represents a refractive index for F-line, Nd represents a refractive index for d-line, and NC represents a refractive index for C-line.

2. A zoom lens according to claim 1, wherein the following expressions are satisfied:

$$1.8 < |\phi11 / \phi12| < 7.0, \text{ and}$$

$$0.5 < |\phi11 / \phi1| < 1.0,$$

where $\phi11$ represents a refractive power of the first lens subunit, $\phi12$ represents a refractive power of the second lens subunit, and $\phi1$ represents a refractive power of the first lens unit.

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3. A zoom lens according to claim 1, wherein the following expression is satisfied:

$$0.020 < \theta_{11a} \times (\theta_{12an} - \theta_{12ap}) < 0.046,$$

where θ_{11a} represents an average value of partial dispersion ratios of the first lens subunit, θ_{12ap} represents an average value of partial dispersion ratios of the at least one positive lens of the second lens subunit, θ_{12an} represents an average value of partial dispersion ratios of the at least one negative lens of the second lens subunit, and partial dispersion ratio θ is defined as,

$$\theta = (N_g - N_F) / (N_F - N_C)$$

where NF represents a refractive index for F-line, N_g represents a refractive index for g-line, and NC represents a refractive index for C-line.

4. A zoom lens according to claim 1, wherein the following expressions are satisfied:

$$0.5 < v_{11a} / (v_{13ap} - v_{13an}) < 4.0, \text{ and}$$

$$0.6 < \phi_{13} / \phi_1 < 1.5,$$

where ϕ_{13} represents a refractive power of the third lens subunit, and v_{13a} represents an average value of Abbe constants of the third lens subunit.

5. A zoom lens according to claim 1, wherein the following expression is satisfied:

$$0.15 < |\phi_1 / \phi_2| < 0.30,$$

where ϕ_2 represents a refractive power of the second lens unit.

6. An image pickup apparatus, comprising:
a zoom lens, comprising, in order from an object side to an image side:
a first lens unit having a positive refractive power;

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a second lens unit having a negative refractive power which moves during zooming;
a third lens unit;
a stop; and
a fourth lens unit having a positive refractive power,

wherein the first lens unit includes, in order from the object side to the image side, a first lens subunit having a negative refractive power which does not move, a second lens subunit having a positive refractive power which moves during focusing, and a third lens subunit having a positive refractive power which does not move,

wherein the first lens subunit is composed of one or more negative lens, and the second lens subunit includes at least one positive lens and at least one negative lens, and

wherein the following expression is satisfied:

$$9 \times 10^6 < v_{11a}^3 \times (v_{12ap} - v_{12an}) < 45 \times 10^6,$$

where v_{11a} represents an average value of Abbe constants of the first lens subunit, v_{12ap} represents an average value of Abbe constants of the at least one positive lens of the second lens subunit, v_{12an} represents an average value of Abbe constants of the at least one negative lens of the second lens subunit, and Abbe constant v is defined as,

$$v = (N_d - 1) / (N_F - N_C)$$

where NF represents a refractive index for F-line, N_d represents a refractive index for d-line, and NC represents a refractive index for C-line; and
an image pickup element for receiving light from the zoom lens.

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